

Q1/

DAOUDI IMANE

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$$CD = \frac{2K_T}{r \cdot D_p \cdot M_{eq} \cdot P(R+LP)}$$

$$CR = \frac{2K_E}{r \cdot D_p}$$

$$H(P) = \frac{\frac{2K_T}{r \cdot D_p \cdot M_{eq} \cdot P(R+LP)}}{1 + \frac{4K_E \cdot K_T}{r^2 \cdot D_p^2 \cdot M_{eq} \cdot P(R+LP)}}$$

Q2/ forme canonique:

$$H(P) = \frac{2K_T \cdot r \cdot D_p}{r^2 \cdot D_p^2 \cdot M_{eq} \cdot P(R+LP) + 4K_E \cdot K_T}$$

$$= \frac{2K_T \cdot r \cdot D_p}{r^2 \cdot D_p^2 \cdot M_{eq} \cdot L P^2 + r^2 \cdot D_p^2 \cdot M_{eq} R P + 4K_E K_T}$$

$$H(P) = \frac{\frac{r \cdot D_p}{2K_E}}{1 + \frac{r^2 \cdot D_p^2 \cdot M_{eq} \cdot R}{4K_E K_T} P + \frac{r^2 \cdot D_p^2 \cdot M_{eq} \cdot L}{4K_E K_T} P^2}$$

$$\omega_n = \sqrt{\frac{4K_E K_T}{r^2 D_p^2 M_{eq} L}} \quad , \quad G = \frac{r D_p}{2K_E}$$

$$\frac{2z}{\omega_n} = \frac{r^2 \cdot D_p^2 \cdot M_{eq} \cdot R}{4K_E K_T}$$

$$z = \frac{1}{2} \times \frac{r^2 \cdot D_p^2 \cdot M_{eq} \cdot R}{4K_E K_T} \times \sqrt{\frac{4K_E K_T}{r^2 \cdot D_p^2 \cdot M_{eq} \cdot L}}$$

$$z = \frac{1}{2} \sqrt{\frac{r^2 \cdot D_p^2 \cdot M_{eq} R^2}{4K_E K_T \cdot L}}$$

$$z = \frac{r D_p R}{4} \sqrt{\frac{M_{eq}}{K_E K_T L}}$$

$$G = 0,03125$$

$$z = 2,37 \Rightarrow z > 1$$

$$\omega_m = 45,25 \text{ rad/s}$$

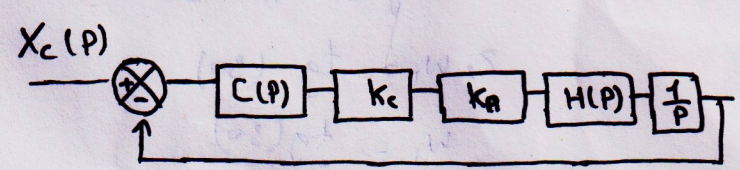
Q3/

on utilise le théorème de Pôles dominants,
on remarque $z \gg \omega_n$

$$\text{d'où: } H(P) \approx \frac{G}{1+z_2 P}$$

$$H(P) = \frac{0,03125}{1+0,1P}$$

Simplification de schéma:



Q4/

$$H_{bo}(P) = C(P) \cdot K_c \cdot K_a \cdot H(P) \cdot \frac{1}{P}$$

$$H_{bo}(P) = \frac{K_c K_a G}{P(1+z_2 P)} \Rightarrow MG = +\infty$$

Q5/

• Marges de gain: $MG = +\infty$

• Marges de phase:

$$MP = -145 + 180 = 35^\circ \Rightarrow k=1$$

Puisque $MP > 0 \Rightarrow$ système stable

Q6/

$$H_{bo}(P) = \frac{K \cdot K_a \cdot K_c \cdot G}{P(1+z_2 P)}$$

$$H_{Bo}(j\omega) = \frac{k \cdot k_a \cdot k_c \cdot G}{j\omega(1 + \tau_2 j\omega)}$$

* Module:

$$|H_{Bo}(j\omega)| = \frac{k \cdot k_a \cdot k_c \cdot G}{\omega \sqrt{1 + (\tau_2 \omega)^2}}$$

+ Argument:

$$\text{Arg}(H_{Bo}(j\omega)) = -90 - \arctg(\tau_2 \omega)$$

$$\left\{ \begin{array}{l} MP = 180 + \text{Arg}(H_{Bo}(j\omega_1)) \\ \text{à } \omega_1 : |H_{Bo}(j\omega_1)| = 1 \end{array} \right.$$

On a.

$$MP = 180 - 90 - \arctg(\tau_2 \omega_1) = 60$$

$$\Leftrightarrow \arctg(\tau_2 \omega_1) = 30$$

$$\tau_2 \omega_1 = \text{tg}(30)$$

$$\omega_1 = \frac{\text{tg}(30)}{\tau_2}$$

$$\omega_1 = 5,77 \text{ rad/s}$$

$$\text{on } |H_{Bo}(j\omega_1)| = 1$$

$$k \frac{k_a k_c G}{\omega_1 \sqrt{1 + (\tau_2 \omega_1)^2}} = 1$$

$$k = \frac{\omega_1 \sqrt{1 + (\tau_2 \omega_1)^2}}{k_a \cdot k_c \cdot G}$$

$$\text{d'où : } k = 0,34$$

Q2/1.

$$\text{on } H_{Bo}(P) = \frac{k \cdot k_a \cdot k_c \cdot G}{P(1 + \tau_2 P)}$$

plus que HBO possède une intégration $\Rightarrow \Sigma_s = 0$

le système est précis.

$$\Sigma_s < 1\%$$

Q8°

$$\begin{aligned} F(P) &= \frac{H_{Bo}(P)}{1 + H_{Bo}(P)} \\ &= \frac{k \cdot k_a \cdot k_c \cdot G}{P(1 + \tau_2 P) + k \cdot k_a \cdot k_c \cdot G} \\ &= \frac{1}{1 + \frac{1}{k \cdot k_a \cdot k_c \cdot G} P + \frac{\tau_2}{k \cdot k_a \cdot k_c \cdot G} P^2} \end{aligned}$$

$$\omega_n = \sqrt{\frac{k_a k_c \cdot k \cdot G}{\tau_2}}$$

$$\frac{2z}{\omega_n} = \frac{1}{k \cdot k_a \cdot k_c \cdot G}$$

$$z = \frac{1}{2} \sqrt{\frac{1}{k_a k_c k \cdot G \cdot \tau_2}}$$

$$z = 0,6$$

$$\omega_n = 8,24 \text{ rad/s}$$

Q9°

$$\text{pour } z = 0,6 \Rightarrow \text{tr}_s\% \cdot \omega_n = 5,2$$

$$\text{tr}_s\% = \frac{5,2}{8,24} = 0,63 \text{ s}$$

$$\text{tr}_s\% = 0,63 \text{ s} < 1 \text{ s}$$

il respect l'exigence sur la rapidité.